

Mason Lecture 9

9/28/06
①

Screw Coords for Differential Twists

Recall def. of Screw

θ = angle of rotation

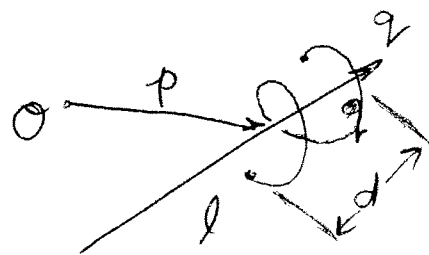
d = length of ~~the~~ translation

l = line of screw axis

$$\rho = p = \text{pitch} = \frac{d}{\theta}$$

$$\text{screw} \triangleq \left(\theta \frac{s}{\|s\|}, \theta \frac{s_0}{\|s\|} \right)$$

$$= \frac{1}{\|q\|} (\theta q, \theta q_0 + dq)$$



Consider differential motion occurring over differential time, dt

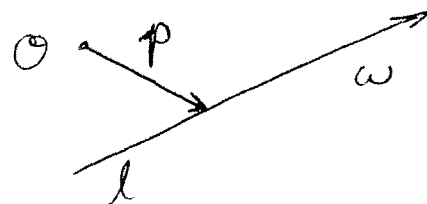
$\theta = \omega dt$, where ω is the angular velocity

Plücker coords $(q, q_0) = (\omega, p \times \omega)$

$$\text{pitch} = \frac{\|\omega\|}{\|p \times \omega\|}$$

~~Screw coords for diff twist:~~

~~$$(s, s_0) = (\omega, p \times \omega)$$~~



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Screw coords for diff. twist: ω plays role of q . ⁽²⁾

$$(s, s_0) = (\omega, p \times \omega + \frac{\|N\|}{\|\omega\|} \omega)$$

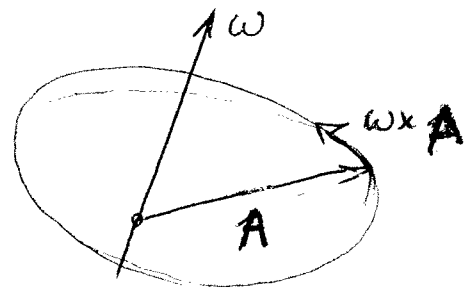
note that N is \parallel to ω (by construction)

$$\therefore N = \frac{\omega}{\|\omega\|}$$

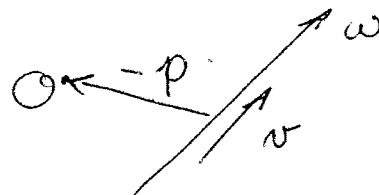
$$(s, s_0) = (\omega, p \times \omega + N)$$

what is the physical interp.?

given a vector A ,
 $\omega \times A =$ velocity
 or time rate of
 change of A



What is
 the twist? $\rightarrow (\omega, \omega \times (-p) + N)$



$$\omega \times -p + N$$

= velocity of point attached to moving body
 that is instantaneously coincident
 with the origin.

Lecture 9 begins here

Kinematic Constraints - First Order


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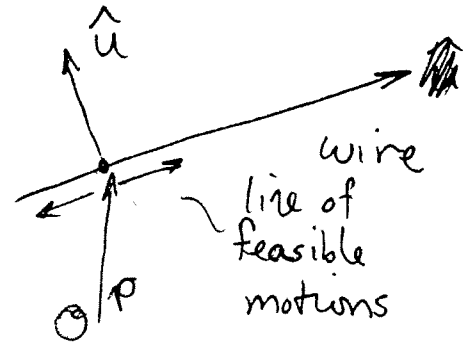
(1)

Let N_p be a point of interest

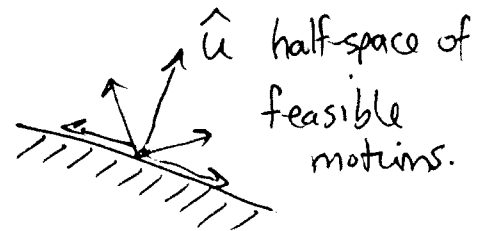
Let \hat{u} be a direction, then

$$\hat{u} \cdot N_p = 0$$

constrains the point to move along the ~~direction~~ 

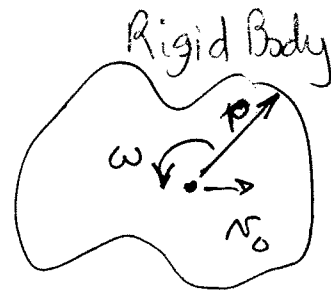


$$\hat{u} \cdot N_p \geq 0$$



Recall $N_p = N_o + \omega \times p$

$$\begin{aligned} \hat{u} \cdot N_p &= \\ &= \hat{u} \cdot N_o + (\omega \times p) \cdot \hat{u} \\ &= \hat{u} \cdot N_o + \underline{(p \times \hat{u})} \cdot \omega \end{aligned}$$



v_o = velocity of origin

Looks like reciprocal product defined for Plücker coordinates

$$(q, q_o) * (p, p_o) = q \cdot p_o + p \cdot q_o$$

Define contact screw

$$(c, c_o) = (\hat{u}, p \times \hat{u})$$

Consideration of constraint gives rise to a "contact screw"

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Kinematic Constraint can now
be written as :

(2)

$$(c, c_0) * (\omega, \nu_0) = c \cdot \nu_0 + c_0 \cdot \omega = 0$$

Call virtual product, because contact screw can be

Definition: Two screws are reciprocal, contrary, or repelling
if the reciprocal product is $= 0$, < 0 , or > 0 .

Bilateral constraints must be reciprocal

Unilateral constraints are reciprocal or repelling

Note:

Every point on ^a rigid body has same ω

Diff twist represents velocity of pt at origin

In (c, c_0) , c represents direction of constraint

c_0 is moment of constraint about origin.

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Example : Contact constraints

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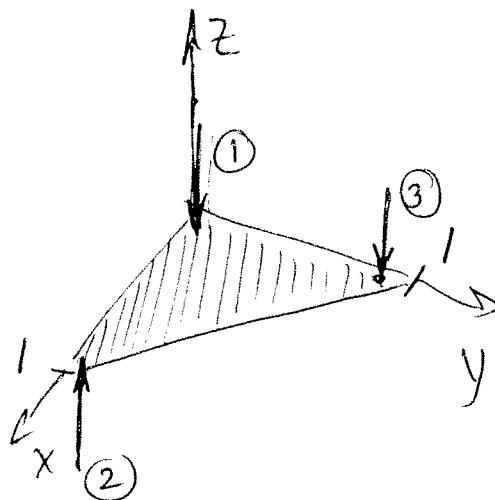
for planar motion

Let contact points
be at :

$$r_1 = (0, 0, 0)$$

$$r_2 = (1, 0, 0)$$

$$r_3 = (0, 1, 0)$$



Contact screws, (C_i, C_{oi}) $i=1,2,3$

① $(\underbrace{0 \ 0 \ -1}_S; \underbrace{0 \ 0 \ 0}_{r \times S = S_0})$

② $(0 \ 0 \ 1; 0 \ -1 \ 0)$

③ $(0 \ 0 \ -1; -1 \ 0 \ 0)$

Recall that moment
about origin = moment
about each of the axes.

Moment between || lines $S=C$
Moment || intersecting " "

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(2)

How can we determine possible motion of "grasped" triangle?

Let $(t, t_0) = (\omega, \nu_0)$ be the diff. twist of the Δ .

Assume bilateral contacts.

$$(t, t_0) \cdot (c_i, c_{0i}) = 0 \quad \forall i=1,2,3.$$

$$t \cdot c_{0i} + t_0 \cdot c_i = 0 \quad i=1,2,3$$

$$c_i \cdot \nu_0 + c_{0i} \cdot \omega = 0$$

reverse to match book examples

$$\begin{bmatrix} c_1 & c_{01} \\ c_2 & c_{02} \\ c_3 & c_{03} \end{bmatrix} \begin{bmatrix} \nu_0 \\ \omega \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$\begin{array}{l} \textcircled{1} \\ \textcircled{2} \\ \textcircled{3} \end{array} \begin{bmatrix} 0 & 0 & -1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & -1 & 0 \\ 0 & 0 & -1 & -1 & 0 & 0 \end{bmatrix} \begin{bmatrix} \nu_x \\ \nu_y \\ \nu_z \\ \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

Det = 1

$$\textcircled{1} \quad -\nu_z = 0$$

$$\textcircled{2} \quad \nu_z - \omega_y = 0 \Rightarrow \omega_y = 0$$

$$\textcircled{3} \quad -\nu_z - \omega_x = 0 \Rightarrow \omega_x = 0$$

Note that ν_x, ν_y, ω_z are unconstrained!
Planar motion.

- 1.) Twist axis direction
 $(t, t_0) = (\omega, \mathcal{N}_0)$

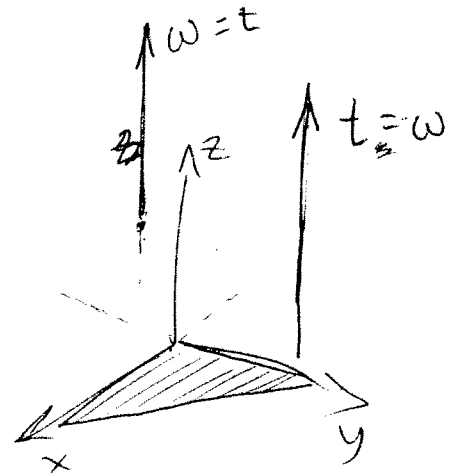
$$t = \omega = \begin{bmatrix} 0 \\ 0 \\ \omega_z \end{bmatrix}$$

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(2.1)

- 2.) Find twist ~~axis~~ pitch

$$(t, t_0) = (\omega, \mathcal{N}_0) = \left(\begin{bmatrix} 0 \\ 0 \\ \omega_z \end{bmatrix}, \begin{bmatrix} \mathcal{N}_{0x} \\ \mathcal{N}_{0y} \\ 0 \end{bmatrix} \right)$$



$$p = \frac{t \cdot t_0}{t \cdot t} = 0$$

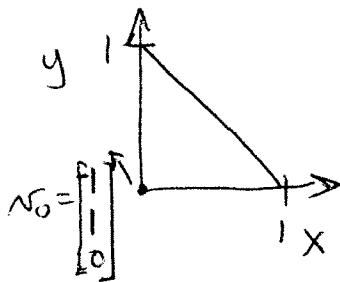
- 3.) Find (closest point on twist axis to origin) (Instantaneous center of rotation)

$$\frac{t \times t_0}{t \cdot t} = \frac{\omega \times \mathcal{N}_0}{\omega \cdot \omega} = \begin{bmatrix} -\mathcal{N}_{0y}/\omega_z \\ \mathcal{N}_{0x}/\omega_z \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} i & j & k \\ 0 & 0 & \omega_z \\ \mathcal{N}_{0x} & \mathcal{N}_{0y} & 0 \end{bmatrix}$$

Let $\omega_z = 1/2$

Let $\mathcal{N}_0 = \begin{bmatrix} -1 \\ 1 \\ 0 \end{bmatrix}$



$$\omega_z \begin{bmatrix} -\mathcal{N}_{0y} \\ \mathcal{N}_{0x} \\ 0 \end{bmatrix}$$

(-2,2) $\cdot \frac{1}{2} = \omega_z$
 twist axis

Suppose we use a different origin?

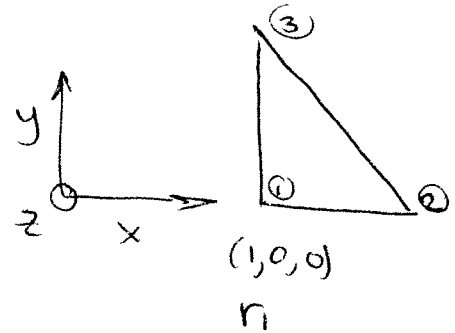
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2.2

Suppose we use a different origin

$$r_1 = (1, 0, 0)$$

$$r_2 = (2, 0, 0)$$

$$r_3 = (1, 1, 0)$$



Contact screws

ξ_{s_1, s_2, s_3} are not changed

$r \times s_i$ is changed by

$$r_{i, \text{new}} = r_{i, \text{old}} + \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

$$\therefore s_{i, \text{new}} = s_{i, \text{old}} + \underbrace{\begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \times s_{i, \text{old}}}_{\Delta s_i}$$

$$\Delta s_{1,3} = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \times \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$$

$$\begin{vmatrix} i + k \\ 1 & 0 & 0 \\ 0 & 0 & -1 \end{vmatrix} = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} \curvearrowright$$

$$\Delta s_2 = -\Delta s_3$$

①	$(0 \ 0 \ -1, \ 0 \ 1 \ 0)$	N_{0x}
②	$(0 \ 0 \ 1, \ 0 \ -2 \ 0)$	N_{0y}
③	$(0 \ 0 \ -1, \ -1 \ 1 \ 0)$	N_{0z}
	$\underbrace{\hspace{10em}}_{\text{Determinant still } \neq 0 = 1}$	w_x
		w_y
		w_z

Check for freedoms.

Same result as before, $N_{0z} = w_x = w_y = 0$

Freedoms: N_{0x}, N_{0y}, w_z

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(2.3)

1. Check twist axis direction

$$\omega = \begin{pmatrix} 0 \\ 0 \\ \omega_z \end{pmatrix} \quad \text{same as before}$$

2. Find pitch

$$\rho = \frac{t \cdot t_0}{t \cdot t} = \frac{\begin{pmatrix} 0 \\ 0 \\ \omega_z \end{pmatrix} \cdot \begin{pmatrix} N_{0x} \\ N_{0y} \\ 0 \end{pmatrix}}{t \cdot t} = 0$$

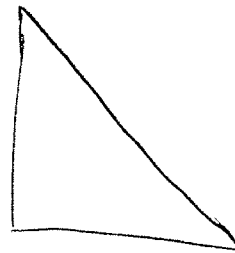
Same
as before.

3. Find closest point on twist axis to origin

Only one difference from before

Since origin was
changed, (N_{0x}, N_{0y})

specifies velocity of ↗



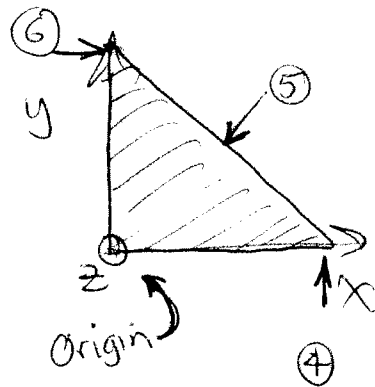
Further constraint in the plane

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(3)

$$\left[\begin{array}{ccc|ccc} 0 & 1 & 0 & 0 & 0 & 1 \\ -\frac{\sqrt{2}}{2} & -\frac{\sqrt{2}}{2} & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & -1 \end{array} \right] \begin{array}{l} N_{ox} \\ N_{oy} \\ N_{oz} \\ \omega_x \\ \omega_y \\ \omega_z \end{array}$$

already eliminated by contacts 1, 2, 3.



Ask: will triangle be able to move?

Can this move?

Assume bilateral constraints

$$\underbrace{\begin{bmatrix} 0 & 1 & 1 \\ -\frac{\sqrt{2}}{2} & -\frac{\sqrt{2}}{2} & 0 \\ 1 & 0 & -1 \end{bmatrix}}_A \begin{bmatrix} N_{ox} \\ N_{oy} \\ \omega_z \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

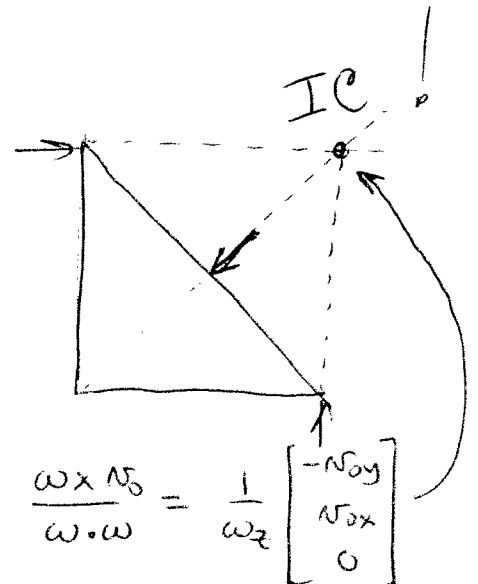
$$\text{Det}(A) = -\frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2} = 0$$

Null Space is 1D

$$\begin{bmatrix} N_{ox} \\ N_{oy} \\ \omega_z \end{bmatrix} = \lambda \begin{bmatrix} 1 \\ -1 \\ 1 \end{bmatrix}, \lambda \in \mathbb{R}$$

location of center of rotation

$$\frac{t \times t_0}{t \cdot t} = \frac{\omega \times N_0}{\omega \cdot \omega} = \frac{1}{\omega_z} \begin{bmatrix} -N_{oy} \\ N_{ox} \\ 0 \end{bmatrix}$$



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(3.1)

Suppose we move frame of representation?

Constraints

$$\underbrace{\begin{bmatrix} 0 & 1 & 2 \\ -\frac{\sqrt{2}}{2} & -\frac{\sqrt{2}}{2} & -\frac{\sqrt{2}}{2} \\ 1 & 0 & -1 \end{bmatrix}}_A \begin{bmatrix} N_{0x} \\ N_{0y} \\ \omega_z \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} N_{0x} \\ N_{0y} \\ \omega_z \end{bmatrix} = \text{Null Sp}(A) \gamma$$

↑ arbitrary scalar

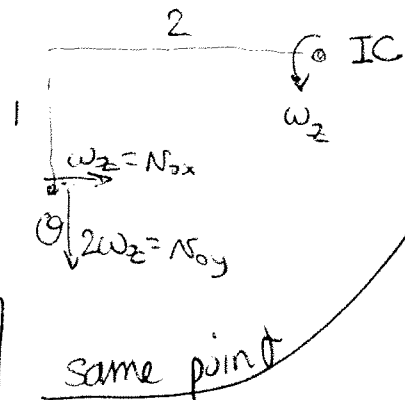
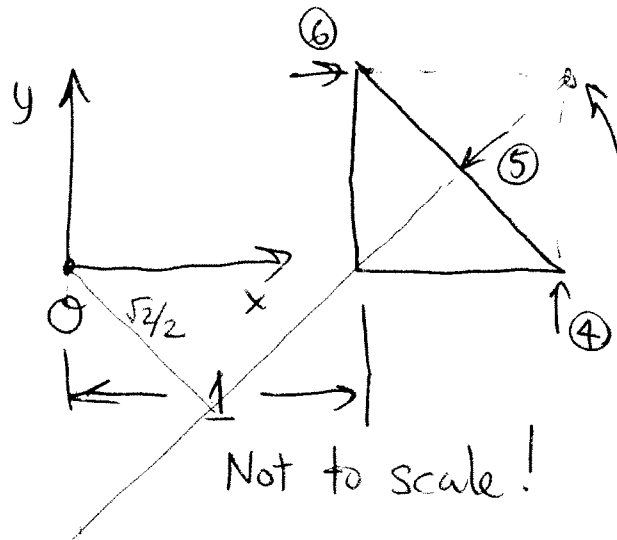
Matlab gives

$$\begin{bmatrix} N_{0x} \\ N_{0y} \\ \omega_z \end{bmatrix} = \begin{bmatrix} 1 \\ -2 \\ 1 \end{bmatrix} \gamma$$

Intuitive Check

∴ Center of rotation is

$$\begin{bmatrix} 2 \\ 1 \\ 0 \end{bmatrix}$$



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Revisit Reuleaux's Method

Repelling screws

$$(c, c_0) * (\omega, \mathcal{N}_0) \geq 0$$

$$(0 \ 1 \ \phi, \ \phi \ \phi \ 0) \begin{bmatrix} \mathcal{N}_{0x} \\ \mathcal{N}_{0y} \\ \mathcal{N}_{0z} \\ \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} \geq 0$$

$$\Rightarrow \mathcal{N}_{0y} \geq 0$$

$\Rightarrow \mathcal{N}_{0x}, \omega_z$ arbitrary

What are IC locations such that $\mathcal{N}_{0y} \geq 0$?

~~$$t \times t_0$$~~

$$\frac{t \times t_0}{t \cdot t} = \begin{bmatrix} -\mathcal{N}_{0y}/\omega_z \\ +\mathcal{N}_{0x}/\omega_z \\ 0 \end{bmatrix}$$

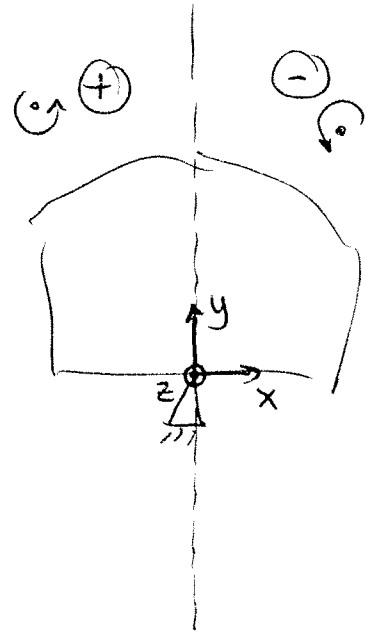
Must have $\mathcal{N}_{0y} > 0$

Case 1: ~~choose~~ $\omega_z > 0, \mathcal{N}_{0y} > 0$

$$\Rightarrow p_x < 0$$

Case 2: $\omega_z < 0, \mathcal{N}_{0y} > 0$

$$\Rightarrow p_x > 0$$



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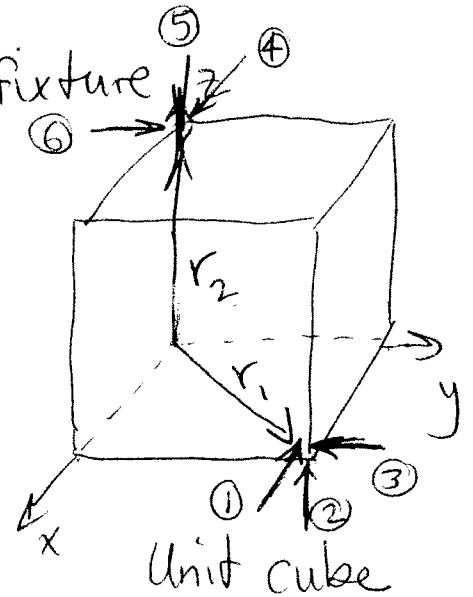
Contact constraint example: grasping

①

Let (c_i, c_{oi})
 Let (s_i, s_{oi}) be the contact screw for
 the i th contact in a grasp/fixture

Let (ω, v_0)
 Let (t, t_0) be the differential
 twist of the object.

Determine instantaneous
 motions allowed by grasp.



$$r_1 = (1, 1, 0)$$

$$r_2 = (0, 0, 1)$$

$s_1 = (-1 \ 0 \ 0)$	$s_{o1} = (0 \ 0 \ 1)$
$s_2 = (0 \ 0 \ 1)$	$s_{o2} = (1 \ -1 \ 0)$
$s_3 = (0 \ -1 \ 0)$	$s_{o3} = (0 \ 0 \ -1)$
$s_4 = (1 \ 0 \ 0)$	$s_{o4} = (0 \ 1 \ 0)$
$s_5 = (0 \ 0 \ -1)$	$s_{o5} = (0 \ 0 \ 0)$
$s_6 = (0 \ 1 \ 0)$	$s_{o6} = (-1 \ 0 \ 0)$

Note: moment about origin = (moment about
 x-axis, y-axis, z-axis)

has
 3 components

Moment between // lines = 0

Moment between intersecting lines = 0

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(2)

Assume constraints are bilateral

differential
Find legal twists if any exist.

$$\begin{array}{l}
 \textcircled{1} \\
 \textcircled{2} \\
 \textcircled{3} \\
 \textcircled{4} \\
 \textcircled{5} \\
 \textcircled{6}
 \end{array}
 \begin{bmatrix}
 -1 & 0 & 0 & 0 & 0 & 1 \\
 0 & 0 & 1 & 1 & 1 & 0 \\
 0 & -1 & 0 & 0 & 0 & -1 \\
 1 & 0 & 0 & 0 & 1 & 0 \\
 0 & 0 & -1 & 0 & 0 & 0 \\
 0 & 1 & 0 & -1 & 0 & 0
 \end{bmatrix}
 \begin{bmatrix}
 N_{ox} \\
 N_{oy} \\
 N_{oz} \\
 \omega_x \\
 \omega_y \\
 \omega_z
 \end{bmatrix}
 =
 \begin{bmatrix}
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0
 \end{bmatrix}$$

A

⑤ $\Rightarrow N_{oz} = 0$

Null space has 1 dimension

$$\text{Null}(A) = \begin{bmatrix} -1 \\ 1 \\ 0 \\ 1 \\ 1 \\ -1 \end{bmatrix}$$

$\left. \begin{matrix} -1 \\ 1 \\ 0 \end{matrix} \right\} N_o = t_o \Rightarrow$
 $\left. \begin{matrix} 1 \\ 1 \\ -1 \end{matrix} \right\} \omega = t$

Note, if origin had been chosen to lie on axis of rotation, then first 3 elements would be zero

corner of cube at origin cannot move up or down.

axis of rotation is along line \parallel to cube diagonal between grasp points.

Point closest to origin

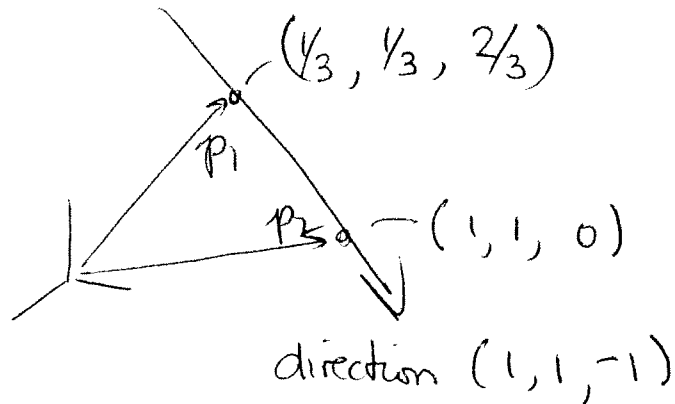
$$\frac{t \cdot t_o}{t \cdot t} = \frac{1}{\sqrt{3}} \begin{vmatrix} i & j & k \\ 1 & 1 & -1 \\ -1 & 1 & 0 \end{vmatrix} = \begin{bmatrix} 1 \\ 1 \\ 2 \end{bmatrix} = \begin{bmatrix} 1/3 \\ 1/3 \\ 2/3 \end{bmatrix}$$

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(3)

Point ~~s~~ seems wrong.

Test to see if it is on axis.



$$\left. \begin{array}{l} p_2 - p_1 = \begin{matrix} i & j & k \\ \frac{2}{3} & \frac{2}{3} & -\frac{2}{3} \end{matrix} \\ \text{cross with } \begin{matrix} i & j & k \\ 1 & 1 & -1 \end{matrix} \end{array} \right\} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

Yes! It is on the line.

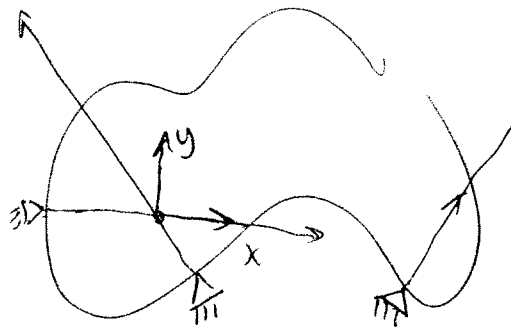
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A final point about screw systems.

Choose ~~for~~ your coordinate frame to make your own life easy.

Results ~~are not so~~

$(c, c_0) \neq (t, t_0)$ are independent of coordinate frame location & orientation!



$$\begin{bmatrix} 1 & 0 & 0 \\ -\frac{1}{2} & \frac{\sqrt{3}}{2} & 0 \\ .8 & .6 & 2 \end{bmatrix}$$

↑ ↑ ↑
 l_i