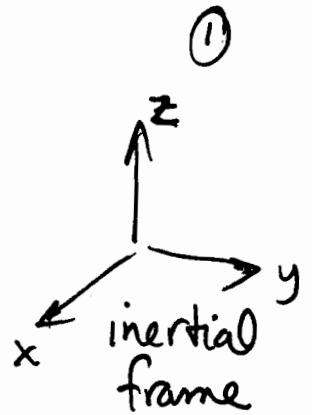


3/21/04

Dynamics of a Particle

$$\text{Let } q = \begin{bmatrix} x \\ y \\ z \end{bmatrix} \quad v = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} N_x \\ N_y \\ N_z \end{bmatrix}$$

Newton's Law

$$\sum \text{forces} = F = \frac{d}{dt}(mv)$$

$$F = m\dot{v} + v\dot{m} \quad \text{Assume } \dot{m} = 0$$

Equations of Motion in First-Order Form

$$\begin{cases} \dot{v} = F/m \\ \dot{q} = v \end{cases}$$

Time Stepping

We want to approx. the solution over the time interval $[a, b]$. (Assume constant time steps.)

$$t_l = a + hl \quad \text{for } l = 0, 1, \dots, M \quad \text{where } h = \frac{b-a}{M}$$

3/21/04

②

Euler's MethodLet $\dot{q} = f(t)$. Taylor expand to approx at t_{l+1}

$$q(t_{l+1}) = q(t_l + h) \cong \frac{df}{dt} h + q(t_l)$$

$$q^{l+1} \cong q^l + \frac{df}{dt} h$$

Explicit if $q^{l+1} = \text{fcn of } q^l$
Implicit otherwise $\frac{df}{dt}$ normally evaluated at t_l , but
this is not required.

Apply to our problem

$$\dot{v} = F/m$$

$$\dot{q} = v$$

Use Euler approximations of \dot{v} and \dot{q}

$$\frac{v^{l+1} - v^l}{h} = F/m \quad \left| \quad F^l/m ? \quad F^{l+1}/m ?$$

$$\frac{q^{l+1} - q^l}{h} = v \quad \left| \quad v^l ? \quad v^{l+1} ?$$

3/21/04

(3)

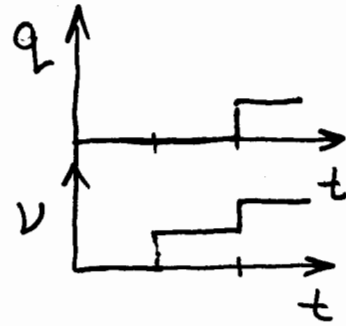
Does it matter where we evaluate F and v ?

$$\left. \begin{aligned} v^{l+1} &= v^l + h \frac{F^l}{m} \\ q^{l+1} &= q^l + h v^l \end{aligned} \right\}$$

← Explicit Method

Everything on RHS is known

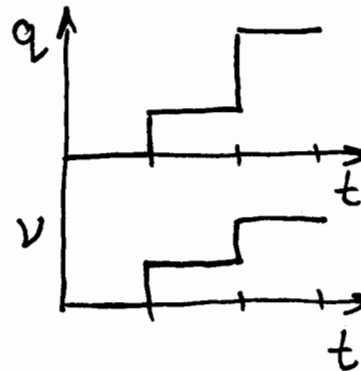
	l	q^l	v^l	Constant F, m, h		
	0	0	0	1	1	1
delayed response	1	0	1	⋮	⋮	⋮
	2	1	2	⋮	⋮	⋮



$$v^{l+1} = v^l + h F/m$$

$$q^{l+1} = q^l + h v^{l+1}$$

	l	q^l	v^l	Constant $F, m, h = 1$		
	0	0	0	1	1	1
extra fast response	1	1	1			
	2	3	2			



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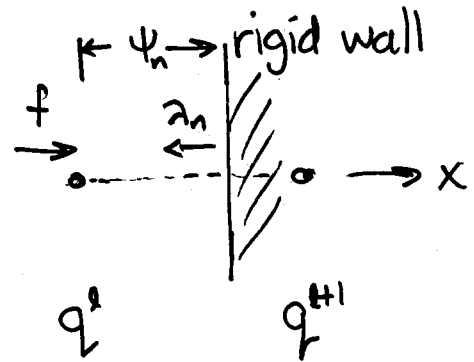
(4)

Consider Dynamics When Collision
is Imminent

Assume 1-dimensional motion.

$$\dot{v} = F/m$$

$$\dot{q} = v$$



Now $F =$ external force + wall force

$$\dot{v} = \frac{1}{m}(f - \lambda_n)$$

$$\dot{q} = v$$

Let $\psi_n =$ dist to wall.

Assume $\lambda_n = 0$ if $\psi_n > 0$
 $\lambda_n \geq 0$ if $\psi_n = 0$
 $\lambda_n > 0$ only if $\psi_n = 0$

~~$\lambda_n \geq 0$~~

$$\lambda_n \geq 0$$

$$\psi_n \geq 0$$

$$\lambda_n \psi_n = 0$$

3/21/04

So now the dynamics are:

(5)

$$\begin{aligned} \dot{v} &= \frac{1}{m}(f - \lambda_n) \\ \dot{q} &= v \\ \text{s.t. } 0 &\leq \lambda_n \perp \psi_n \geq 0 \end{aligned}$$

← complementarity constraint

Suppose velocity is high enough so that particle will bounce.

Then apply an impact model when particle reaches wall.

Newton's Hypothesis

$$v(t_c^+) = -v(t_c^-)e$$

inelastic elastic
 $0 \leq e \leq 1$

where e is known as the coeff. of rest.

3/21/04

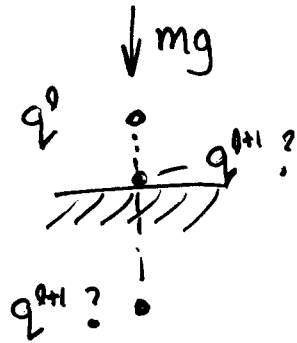
(6)

Suppose collision is inelastic or particle will not bounce off by much.

$$v^{l+1} = v^l + (g + \lambda_n/m)h$$

$$q^{l+1} = q^l + h v^l$$

$$0 \leq \lambda_n \perp \Psi_n \geq 0$$



We want to prevent penetration

Notice that v^l is not biased by contact force, but v^{l+1} is!

\therefore To prevent q^{l+1} from penetrating, we should use v^{l+1} in $q^{l+1} = q^l + h v^{l+1}$.

Now make complementarity constraint valid.

Goal: make system consistent at end of time step.

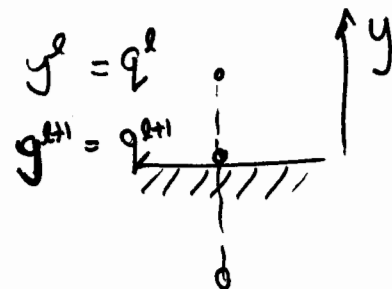
3/21/04

(7)

$$v^{l+1} = v^l + h \left(\frac{\lambda_n^{l+1}}{m} - g^{l+1} \right)$$

$$q^{l+1} = q^l + h v^{l+1}$$

$$0 \leq \lambda_n^{l+1} \perp q^{l+1} \geq 0$$



Substituting first two eqs into third

$$0 \leq \lambda_n^{l+1} \perp \underbrace{\lambda_n^{l+1} \left(\frac{h^2}{m} \right) + q^l + h v^l - g h^2}_{f(\lambda_n^{l+1})} \geq 0$$

Find Solution, \ni $\boxed{\begin{array}{l} \lambda_n^{l+1} = 0 \\ f(\lambda_n^{l+1}) \geq 0 \end{array}} \Bigg| \boxed{\begin{array}{l} f(\lambda_n^{l+1}) = 0 \\ \lambda_n^{l+1} \geq 0 \end{array}}$

OR

Let $m = h = g = 1$, $v^l = -4$ $q^l = 1$

$$0 \leq \lambda_n^{l+1} \perp \lambda_n^{l+1} + \underbrace{1}_{q^l} - \underbrace{4}_{v^l} - \underbrace{1}_{g} \geq 0$$

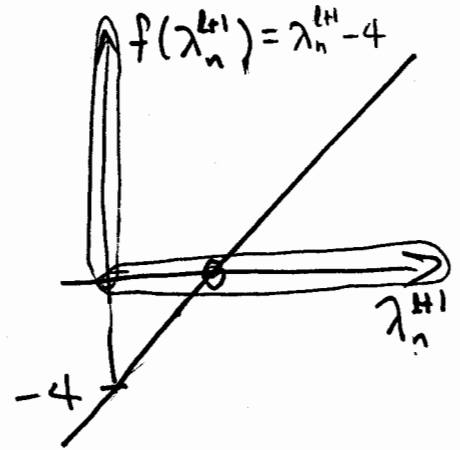
3/21/04

(8)

$$0 \leq \lambda_n^{l+1} \perp \lambda_n^{l+1} - 4 \geq 0$$

Unique Solution

$$\boxed{\lambda_n^{l+1} = 4}$$



Interpretation of solution

Substitute Back in:

$$v^{l+1} = -4 + 1(4 - 1) = -1$$

$$q^{l+1} = 1 + 1(-1) = 0$$

Enough impulse was applied to prevent penetration at end of current time step, BUT NOT ENOUGH TO REMOVE ALL APPROACH VELOCITY!

Next time step

$$0 \leq \lambda_n^{l+2} \perp \lambda_n^{l+2} + \overset{q^l=0}{(-1)} - \overset{g}{1} \geq 0$$

↑
dist covered in $h=1$ at v^{l+1}

←
dist that would be covered by grav. accel in $h=1$.

3/21/04

(9)

$$\therefore \lambda_n^{l+2} = 2$$

We see it takes two time steps to fully resolve a collision.

l	q^l	v^l	λ_n^{l+2}
l	1	-4	0
$l+1$	0	-1	4
$l+2$	0	0	2
$l+3$	0	0	1
\vdots	\vdots	\vdots	\vdots

= mg



3/22/04

(10)

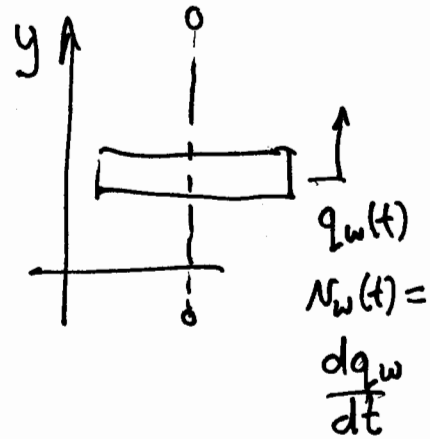
Suppose wall is moving as $q_w(t)$

$$\Psi_n(q, t) = y - q_w(t) \geq 0$$

Discretize

$$\frac{\Psi_n^{k+1} - \Psi_n^k}{h} = \frac{\partial \Psi_n}{\partial q} \underbrace{\frac{q^{k+1} - q^k}{h}}_{v^{k+1}} + \frac{\partial \Psi_n}{\partial t}$$

evaluate where?



$$\Psi_n^{k+1} \approx \underbrace{\Psi_n^k}_{\substack{\uparrow \\ \text{when negative} \\ \text{this term acts to} \\ \text{stabilize the constraint}}} + ((1) v^{k+1} - v_w(t)) h$$

↑ if given fn of time, then could use v_w^{k+1} .

Rewrite LCP

$$v^{k+1} = v^k + h \left(\frac{\lambda_n^{k+1}}{m} - g \right)$$

$$q^{k+1} = q^k + h v^{k+1}$$

$$0 \leq \lambda_n^{k+1} \perp \Psi_n^{k+1} \geq 0$$

3/22/04

(11)

Substitute

$$0 \leq \lambda_n^{l+1} \perp \underbrace{q_l^l - q_\omega^l}_{\psi_n^l} + h(\nu^{l+1} - \nu_\omega) \geq 0$$

$$0 \leq \lambda_n^{l+1} \perp q_l^l - q_\omega^l + h \left[\nu^l + h \left(\frac{\lambda_n^{l+1}}{m} - g \right) - \nu_\omega \right] \geq 0$$

$$\text{Let } h = m = g = 1 \quad \begin{array}{ll} q_l^l = 1 & \nu^l = -4 \\ q_\omega^l = 0 & \nu_\omega^l = 0.5 \end{array}$$

$$0 \leq \lambda_n^{l+1} \perp 1 - 0 + 1 \left[-4 + 1 \left(\frac{\lambda_n^{l+1}}{1} - 1 \right) - \frac{1}{2} \right] \geq 0$$

$$0 \leq \lambda_n^{l+1} \perp \lambda_n^{l+1} - 4.5 \geq 0$$

$$\underline{\lambda_n^{l+1} = 4.5}$$

$$\nu^{l+1} = -4 + \frac{1}{1} 4.5 - 1 = \underline{-0.5} = \nu^{l+1} \quad \leftarrow \text{still has rel. vel. into surf}$$

$$q_l^{l+1} = 1 - 1 \cdot 0.5 = \underline{+0.5} = q_l^{l+1} \quad \leftarrow \text{on surface}$$

$$\text{since } q_\omega^{l+1} = q_\omega^l + h \nu_\omega = 0.5 \quad \leftarrow$$

3/22/04

(12)

Next time step

$$0 \leq \lambda_n^{l+2} \perp q_l^{l+1} - q_l^{l+1} + h(\nu^{l+1} + \frac{h}{m} \lambda_n^{l+2} - hg - N_w) \geq 0$$

$$0 \leq \lambda_n^{l+2} \perp \cancel{0.5} - \cancel{0.5} + 1(-0.5 + \lambda_n^{l+2} - 1 - \cancel{0.5}) \geq 0$$

$$0 \leq \lambda_n^{l+2} \perp \lambda_n^{l+2} - 2.0 \geq 0$$

$$\underline{\lambda_n^{l+2} = 2.0}$$

$$\nu^{l+2} = -0.5 + 1(2.0 - 1) = \underline{0.5} = \nu^{l+2}$$

$$q_l^{l+2} = \cancel{0.5} + 1 \cdot 0.5 = \underline{1.0} = q_l^{l+2}$$

Future time steps will have $\lambda_n^{l+j} = 1$ for $j > 2$

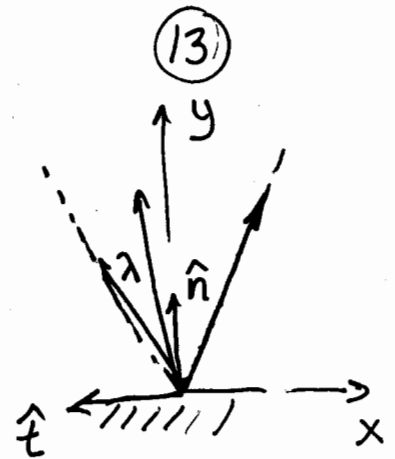
l	ψ_n^l	ν^l	λ_n^l
l	1	-4	0
$l+1$	0	-0.5	4.5
$l+2$	0	0.5	2
$l+3$	0	0.5	1
	\vdots	\vdots	\vdots

How do we add
Add Friction?

3/22/04

Coulomb's Law

Let velocity of particle be $\begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} -N_t \\ N_n \end{bmatrix}$
with position $\begin{bmatrix} 0 \\ 0 \end{bmatrix}$



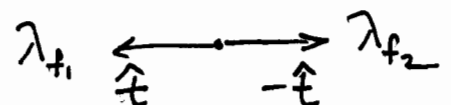
Let λ_n be the normal component of contact force, $\lambda_n \geq 0$
 λ_t be the tangential " " " " in \hat{t} direction

Coulomb's Law is given by:

$\lambda_t = -\mu\lambda_n$	if $\dot{x} < 0$ $N_t > 0$	$\dot{x} < 0$
$-\mu\lambda_n \leq \lambda_t \leq \mu\lambda_n$	if $N_t = 0$	$\dot{x} = 0$
$\lambda_t = \mu\lambda_n$	if $N_t < 0$	$\dot{x} > 0$

Let's divide friction force into positive and negative parts

$\lambda_t = \lambda_{f_1} - \lambda_{f_2}$
st. $\lambda_{f_1}, \lambda_{f_2} \geq 0$



3/22/04

(14)

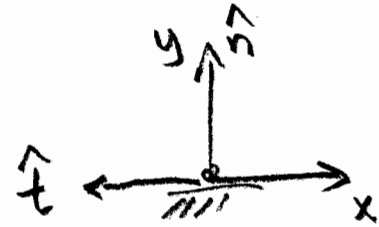
We need something to differentiate between sliding and rolling.

Introduce ^{nonnegative} slack variable s that represents sliding speed.

$$s \geq 0$$

$$N_{f_1} = N_t = -\dot{x}$$

$$N_{f_2} = -N_t = \dot{x}$$



$$v = \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix}$$

Note that this is a wrench matrix $W_f^T \begin{bmatrix} -1 & 0 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} + \begin{bmatrix} s \\ s \end{bmatrix} \geq 0$

$$\left. \begin{array}{l} -\dot{x} + s \geq 0 \\ \dot{x} + s \geq 0 \end{array} \right\} \begin{array}{l} s \geq \dot{x} \\ s \geq -\dot{x} \end{array} \quad s \geq |\dot{x}|$$

if $|\dot{x}| > 0$, then $s > 0$

Depending on which constraint is tight, we can eliminate one friction force.

$$0 \leq \begin{bmatrix} \lambda_{f_1} \\ \lambda_{f_2} \end{bmatrix} \perp \begin{bmatrix} -1 & 0 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} + \begin{bmatrix} s \\ s \end{bmatrix} \geq 0$$

If both are loose we eliminate both. But can't do that.

3/22/04

Sliding Cases

(15)

If $\dot{x} > 0$, then some friction must be active

$$0 \leq \overleftarrow{\lambda}_{f_1} \perp -\dot{x} + s \geq 0$$

$$0 \leq \overrightarrow{\lambda}_{f_2} \perp \dot{x} + s \geq 0$$

$$\dot{x} + s > 0 \therefore \lambda_{f_2} = 0$$

(sliding right \Rightarrow friction force component toward right is zero)

~~≡~~ ≡ Coulomb's law says

$$\lambda_{f_1} = \mu \lambda_n \Rightarrow \overrightarrow{\lambda}_{f_1} - \dot{x} + s = 0$$

$$\Rightarrow s = \dot{x}$$

If $\dot{x} < 0$,

$$0 \leq \lambda_{f_1} \perp -\dot{x} + s \geq 0 \Rightarrow s - \dot{x} > 0 \therefore \lambda_{f_1} = 0$$

$$0 \leq \lambda_{f_2} \perp \dot{x} + s \geq 0$$

$$\therefore \lambda_{f_2} = \mu \lambda_n \Rightarrow s = -\dot{x}$$

But Nothing Here Ensures $\lambda_{f_i} = \mu \lambda_n$!

3/22/04

Since One of $\lambda_{f_1}, \lambda_{f_2}$ is zero, try:

(16)

$$0 \leq s \perp \mu \lambda_n - \lambda_{f_1} - \lambda_{f_2} \geq 0$$

$$0 \leq \begin{bmatrix} \lambda_{f_1} \\ \lambda_{f_2} \end{bmatrix} \perp \begin{bmatrix} -1 & 0 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} + \begin{bmatrix} s \\ s \end{bmatrix} \geq 0$$

Case: Rolling / Sticking ($\dot{x} = 0$)

$$0 \leq \lambda_{f_1} \perp \cancel{-\dot{x}} + s \geq 0 \quad \text{redundant} \quad (1)$$

$$0 \leq \lambda_{f_2} \perp \cancel{+\dot{x}} + s \geq 0 \quad (2)$$

$$0 \leq s \perp \mu \lambda_n - \lambda_{f_1} - \lambda_{f_2} \geq 0 \quad (3)$$

If $s > 0$, then ^{from (1) (2)} $\lambda_{f_1} = \lambda_{f_2} = 0$

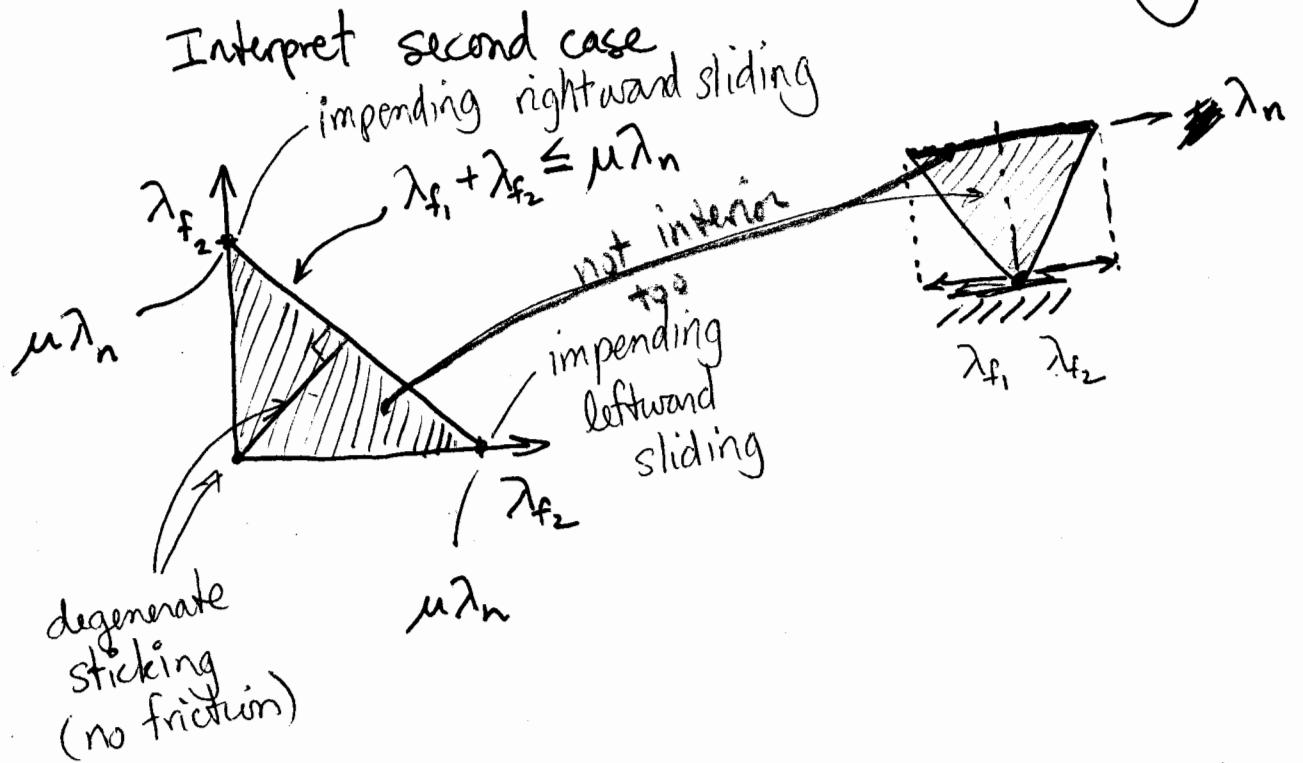
from (3) $\mu \lambda_n = 0$

Not!
Consistent, but
~~s not interpreted~~
~~as sliding velocity~~

If $s = 0$, then from (1) & (2), $\lambda_{f_1}, \lambda_{f_2} \geq 0$
from (3) $\mu \lambda_n - \lambda_{f_1} - \lambda_{f_2} \geq 0$

3/22/04

(17)



Summary: If $\dot{x} = 0$, then $s = 0$ is only consistent case, and friction force must be within cone.

Case Sliding $\dot{x} \neq 0$,

$$0 \leq \lambda_{f_1} \perp -\dot{x} + s \geq 0 \quad (1)$$

$$0 \leq \lambda_{f_2} \perp \dot{x} + s \geq 0 \quad (2)$$

$$0 \leq s \perp \mu \lambda_n - \lambda_{f_1} - \lambda_{f_2} \geq 0 \quad (3)$$

Since $s = |\dot{x}|$
 $s \geq \dot{x}$
 $s \geq -\dot{x}$, $s > 0$

3/22/04

(18)

Assume $\dot{x} > 0$

$$(3) \Rightarrow \mu \lambda_n = \lambda_{f_1} + \lambda_{f_2} \quad \text{which is} > 0$$

\therefore at least one of λ_{f_i} must be > 0

Of $-\dot{x} + s$ and $\dot{x} + s$, only the first can be $= 0$.

$$\therefore \dot{x} = s \quad \text{and} \quad \underline{\lambda_{f_1}} \geq 0 \quad \leftarrow \text{eq. (1)}$$

$$\text{Eq(2)} \Rightarrow \text{since } \dot{x} + s > 0, \quad \underline{\lambda_{f_2}} = 0$$

$$\therefore \boxed{\mu \lambda_n = \lambda_{f_1}}$$

Consistent w/ Friction Law!

Step

3/25/04

Equality Constraints

$$\Theta_i(q, t) = 0 \quad i=1, 2, \dots$$

Why joints & quaternion length constr.

Taylor Expand... (drop i subscript)

$$\Theta(q + \Delta q, t + h) = \Theta^{k+1}$$

$$\Theta(q, t) = \Theta^l$$

$$\Theta^{k+1} = \Theta^l + \frac{\partial \Theta}{\partial q} \Delta q + \frac{\partial \Theta}{\partial t} h$$

$$\Theta^{k+1} = \Theta^l + \frac{\partial \Theta}{\partial q} (q^{k+1} - q^l) + \frac{\partial \Theta}{\partial t} h$$

should be zero
but is not quite

But Θ^{k+1} should equal $\Theta^l = 0$

But Θ^l will not be exactly 0, so keep it

$$0 = \frac{\partial \Theta}{\partial q} v^{k+1} + \frac{\partial \Theta}{\partial t} + \Theta^l / h$$

↑
kinematic

↑
constraint
stabilization

It was natural to put normal contact conditions into the form of a C.P. We now want to extend and include friction if possible. 4/26/03
Complementarity Problems (1.1)

Let w and z be vectors of length n . Further, let $w(z)$ be a given function. The complementarity problem is, find z satisfying:

$$z \geq 0, \quad w(z) \geq 0, \quad w^T(z) z = 0$$

$$\boxed{0 \leq z \perp w(z) \geq 0}$$

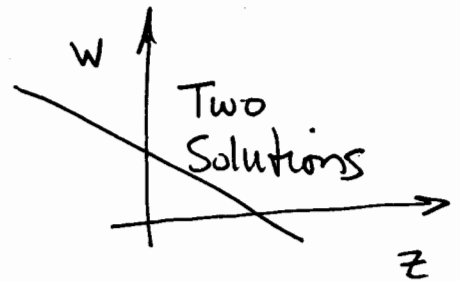
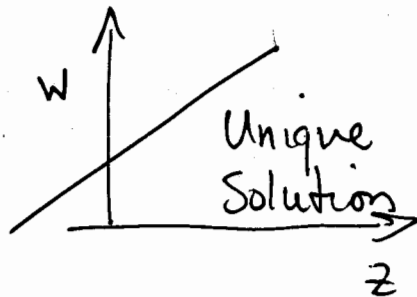
Linear Complementarity Problem (LCP)

If $w(z)$ is defined as

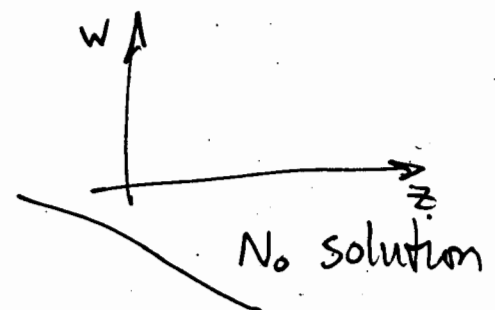
$$w(z) = Fz + f$$

where $F \in \mathbb{R}^{n \times n}$ and $f \in \mathbb{R}^n$ are given constants

LCP of Size 1



The LCP has a unique solution if F is a P-matrix and Lemke's alg. is guaranteed to find a soln. in finite time.



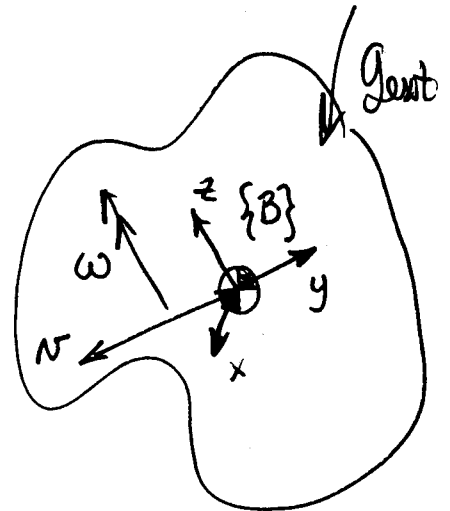
Generalize to Spatial Case
with varying contact types

3/22/04

(19)

ton: $\sum f_i = m \mathbf{I}_{(3 \times 3)} \mathbf{a}$

or: $\sum \mathbf{n}_i = \sum \mathbf{r}_i \times \mathbf{f}_i$
 $= \mathbf{J} \boldsymbol{\alpha} + \boldsymbol{\omega} \times \mathbf{J} \boldsymbol{\omega}$



where $\mathbf{a} = \dot{\mathbf{v}}$, $\mathbf{v} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \\ \dots \\ \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$, $\mathbf{q} = \begin{bmatrix} x \\ y \\ z \\ e_0 \\ e_1 \\ e_2 \\ e_3 \end{bmatrix}$

$\boldsymbol{\omega} = \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$

$e_0^2 + e_1^2 + e_2^2 + e_3^2 = 1$

$M \dot{\mathbf{v}} = \begin{bmatrix} \sum f_i \\ \dots \\ \sum \mathbf{r}_i \times \mathbf{f}_i \end{bmatrix} + \begin{bmatrix} \mathbf{0}_{3 \times 1} \\ \dots \\ -\boldsymbol{\omega} \times \mathbf{J} \boldsymbol{\omega} \end{bmatrix}$ ~~to NFAA~~

where $M = \text{diag}(m \mathbf{I}_{3 \times 3}, \mathbf{J})$

M is P.D. & symmetric

Rotational Kinematics

3/22/04

(20)

$$\dot{q} = G(q) v$$

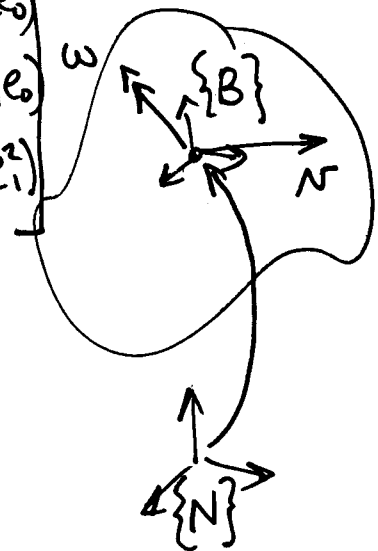
where $G = \begin{bmatrix} I_{(3 \times 3)} & 0 \\ 0 & B(q)_{(4 \times 3)} \end{bmatrix}_{(7 \times 6)}$

$$G^T G = I_{(6 \times 6)}$$

$$B(q) = \begin{bmatrix} -e_1 & -e_2 & -e_3 \\ e_0 & -e_3 & e_2 \\ e_3 & e_0 & -e_1 \\ -e_2 & e_1 & e_0 \end{bmatrix} \frac{1}{2}$$

$$\begin{bmatrix} \dot{e}_0 \\ \dot{e}_1 \\ \dot{e}_2 \\ \dot{e}_3 \end{bmatrix} = B(q) \begin{bmatrix} {}^B \omega_x \\ {}^B \omega_y \\ {}^B \omega_z \end{bmatrix}$$

$${}^N_B R(q) = \begin{bmatrix} 1 - 2(e_2^2 + e_3^2) & 2(e_1 e_2 - e_0 e_3) & 2(e_1 e_3 + e_2 e_0) \\ 2(e_1 e_2 + e_3 e_0) & 1 - 2(e_1^2 + e_3^2) & 2(e_2 e_3 - e_1 e_0) \\ 2(e_1 e_3 - e_0 e_2) & 2(e_2 e_3 + e_1 e_0) & 1 - 2(e_2^2 + e_1^2) \end{bmatrix} \omega$$



$$\underline{\underline{{}^B \omega = {}^B_N R^N \omega}}$$

$$\underline{\underline{\dot{e} = B^B \omega}}$$

RBD w/ no Contact or Ext. Wrenches

3/22/04

20.1

$$M\dot{v} = \begin{bmatrix} \text{---} \frac{O(\beta \times 1)}{\omega \times J \omega} \end{bmatrix}_{(6 \times 1)} + \begin{bmatrix} F \\ N \end{bmatrix}$$

$$\dot{q} = G(q)v$$

$$e_0^2 + e_1^2 + e_2^2 + e_3^2 - 1 = 0$$

Break up equations to use ODE45 (or similar).

~~$$m\dot{v} = F$$

$${}^B J \dot{\omega} = {}^B N - \omega \times {}^B J \omega$$

$$\dot{x} = v$$

$$\dot{e} = B \omega$$~~

$$\dot{v} = F/m$$

$${}^B J \dot{\omega} = N - \omega \times {}^B J \omega \Rightarrow$$

$$\dot{x} = v$$

$$\dot{e} = B \omega$$

$${}^N \dot{v} = {}^N F/m$$
~~$${}^B \dot{\omega} = {}^B J^{-1} ({}^B N - \omega \times {}^B J \omega)$$~~

$${}^N \dot{\omega} = {}^N R {}^B J^{-1} ({}^B N - \omega \times {}^B J \omega)$$

$${}^N \dot{x} = {}^N v$$

$$\dot{e} = B \omega$$